

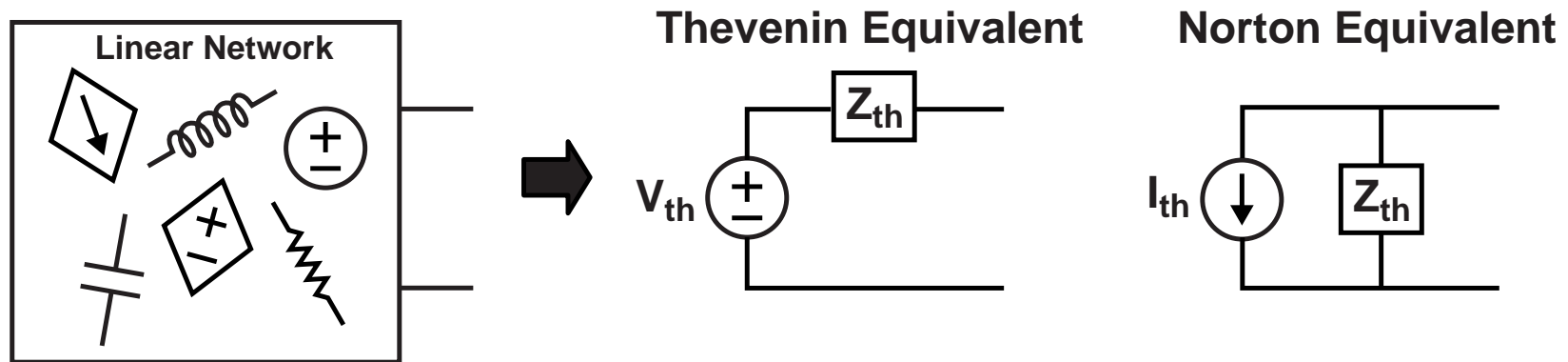
***Analysis and Design of Analog Integrated Circuits***  
***Lecture 2***

***Two-Port Models, Frequency Response***

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**January 25, 2011**

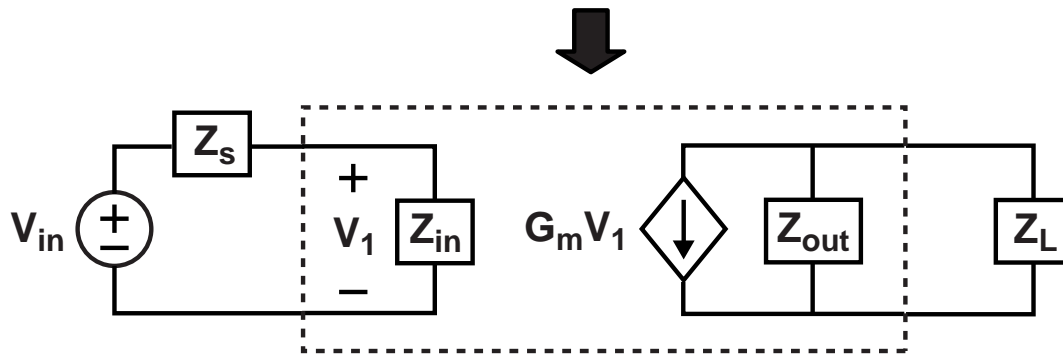
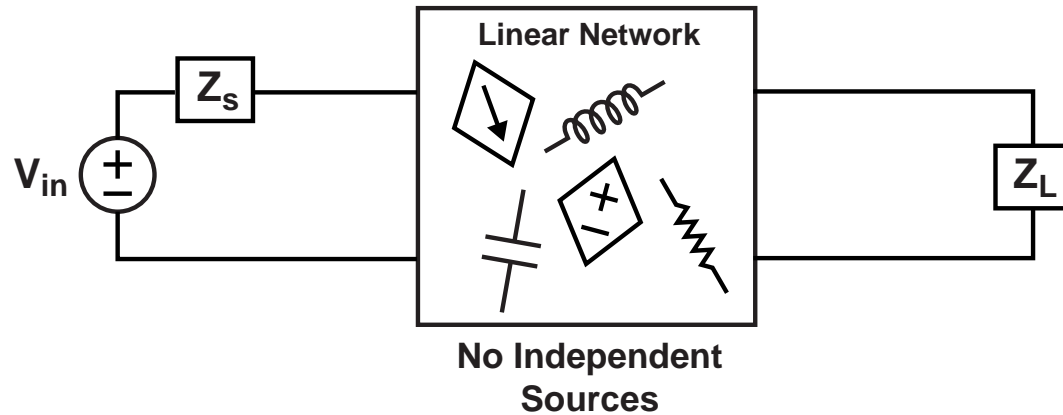
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# Review: Basics of One-Port Modeling

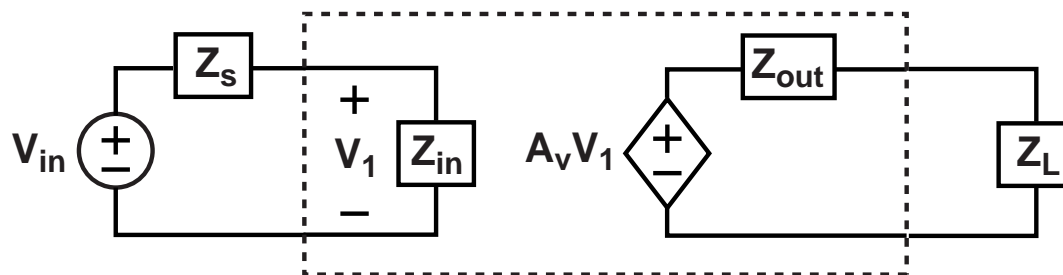


- $V_{th}$  computed as open circuit voltage at port nodes
- $I_{th}$  computed as short circuit current across port nodes
- $Z_{th}$  computed as  $V_{th}/I_{th}$ 
  - All independent voltage and current sources are set to zero value

# Basics of Two-Port Modeling (Unilateral)

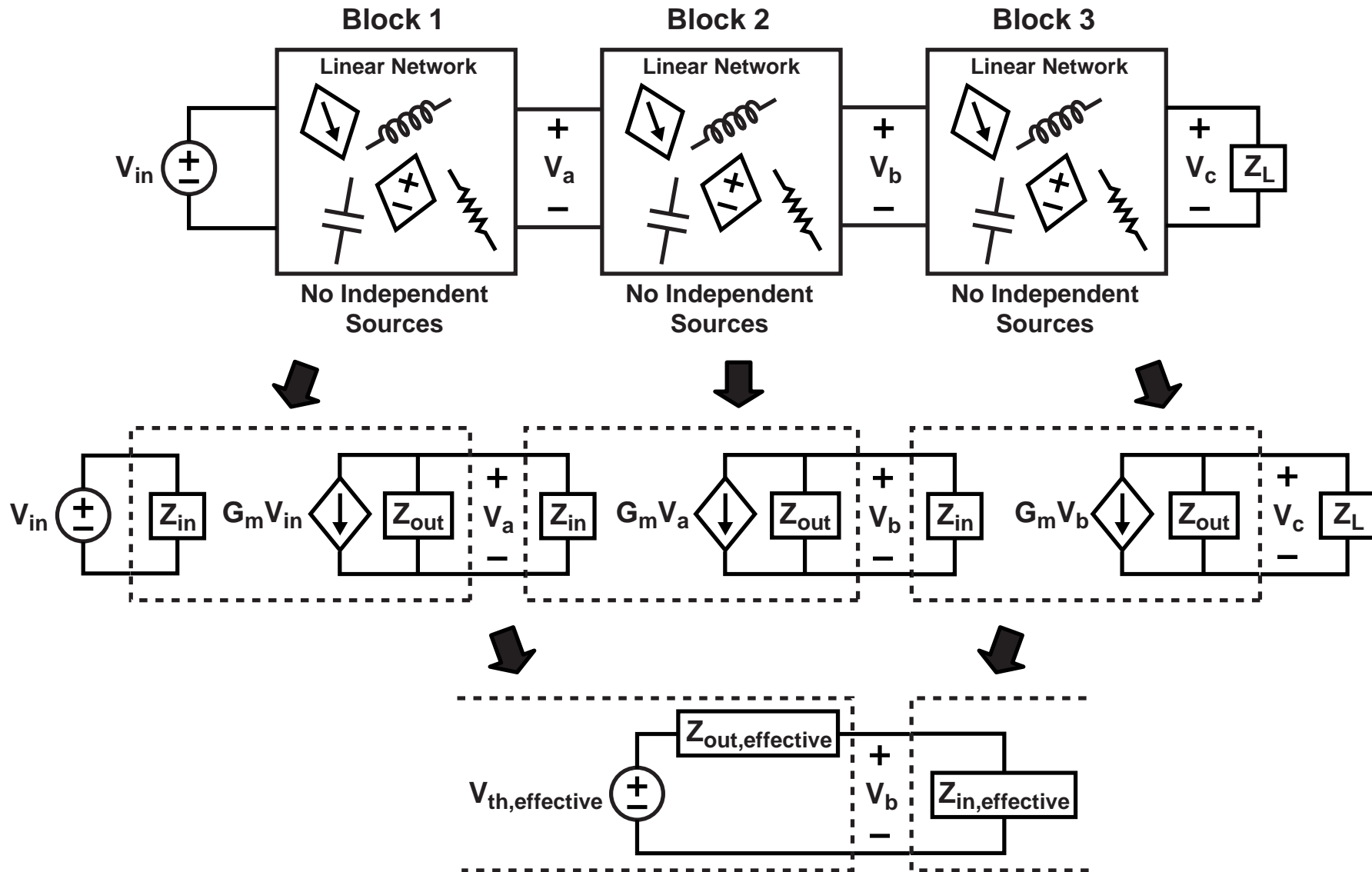


OR



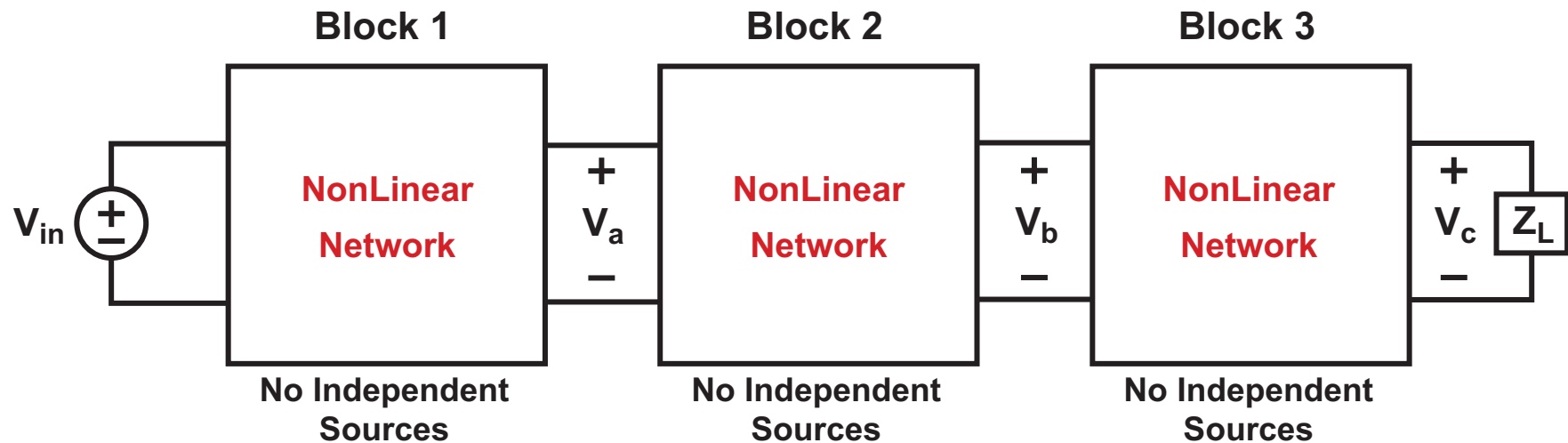
- We now include a dependent current or voltage source
- $Z_{in}$ 
  - Solve using 1-Port analysis at input
- $Z_{out}$ 
  - Solve using 1-Port analysis at output with  $V_1 = 0$
- $G_M$ 
  - Short circuit output current as a function of  $V_1$
- $A_v$ 
  - Open circuit output voltage as a function of  $V_1$

# Analysis of Cascaded Blocks



**Analysis carried out without solving simultaneous equations!**

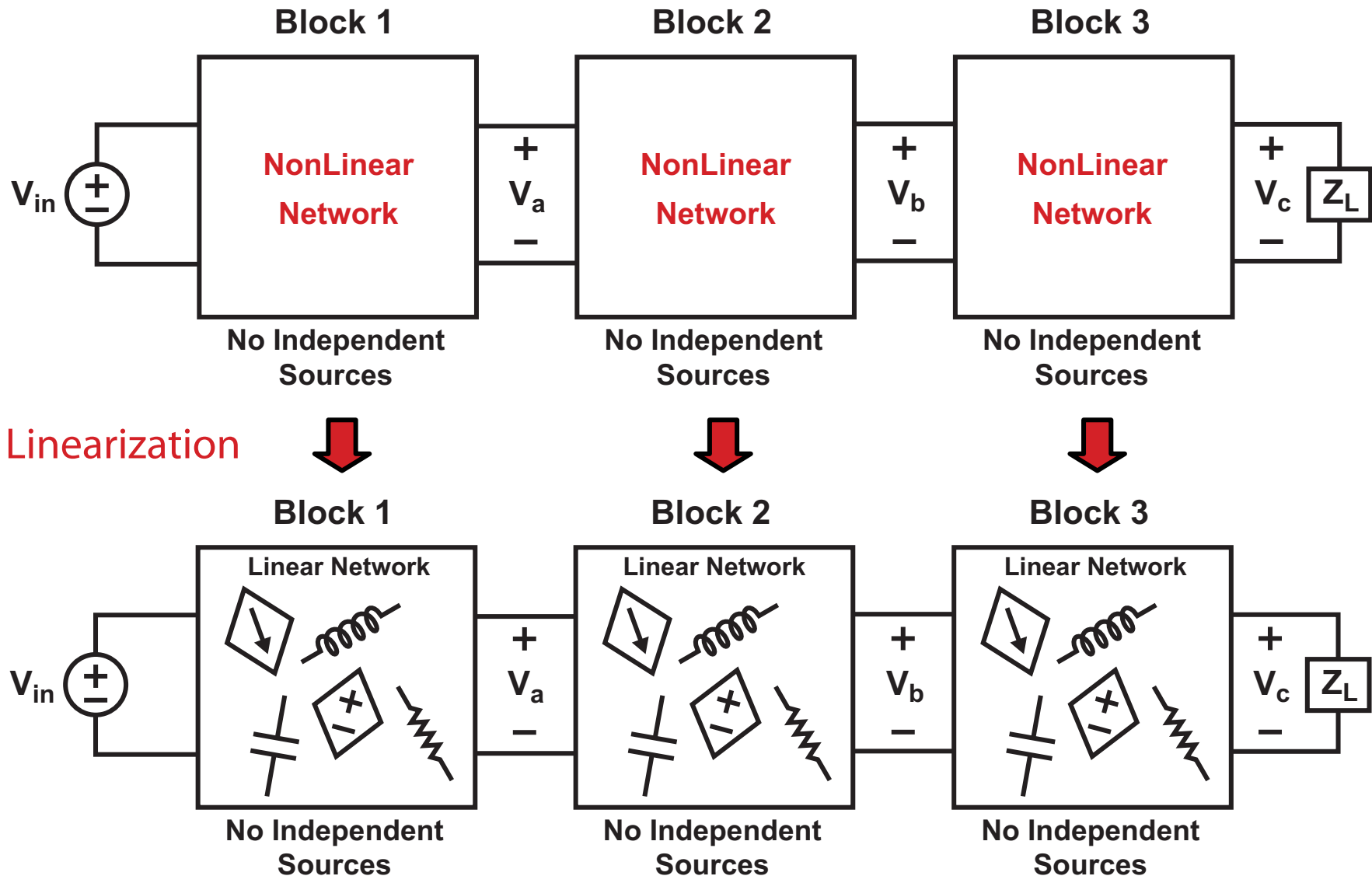
## Problem: Most Circuits are Very Nonlinear!



- Thevenin/Norton modeling only applies to linear networks
- Direct analysis of nonlinear networks is challenging

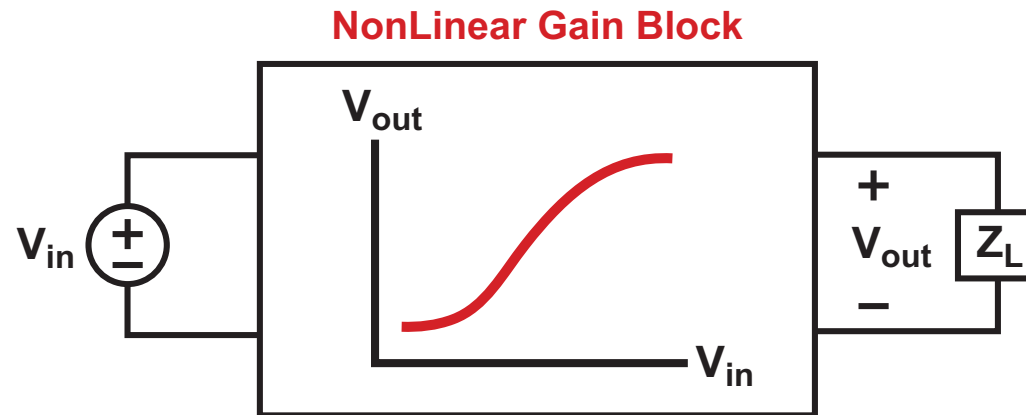
Can we still leverage two-port modeling?

# Small Signal Modeling Allows Us to Linearize



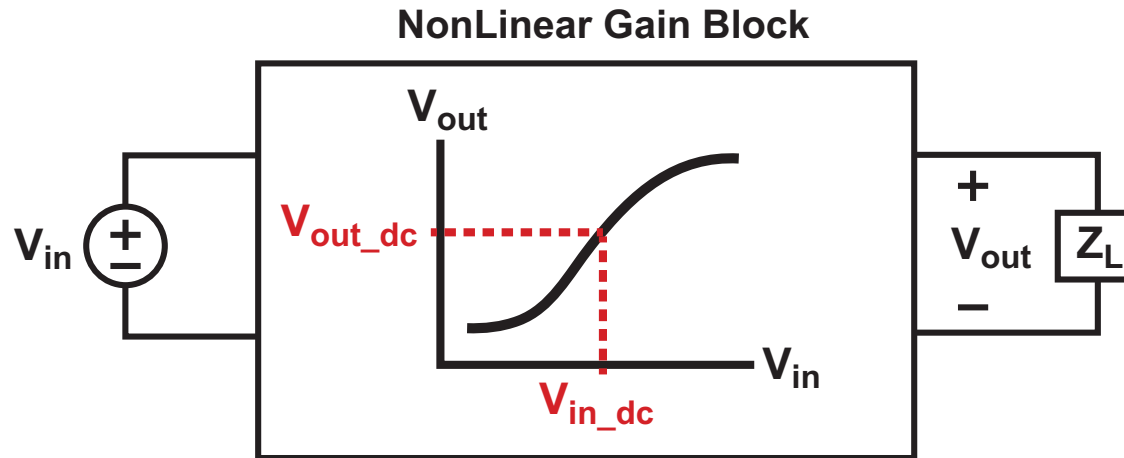
**Small signal model is only valid about a specific operating point**

# Small Versus Large Signal Modeling



- Sketch  $V_{out}$  versus  $V_{in}$  as the amplitude of  $V_{in}$  is increased

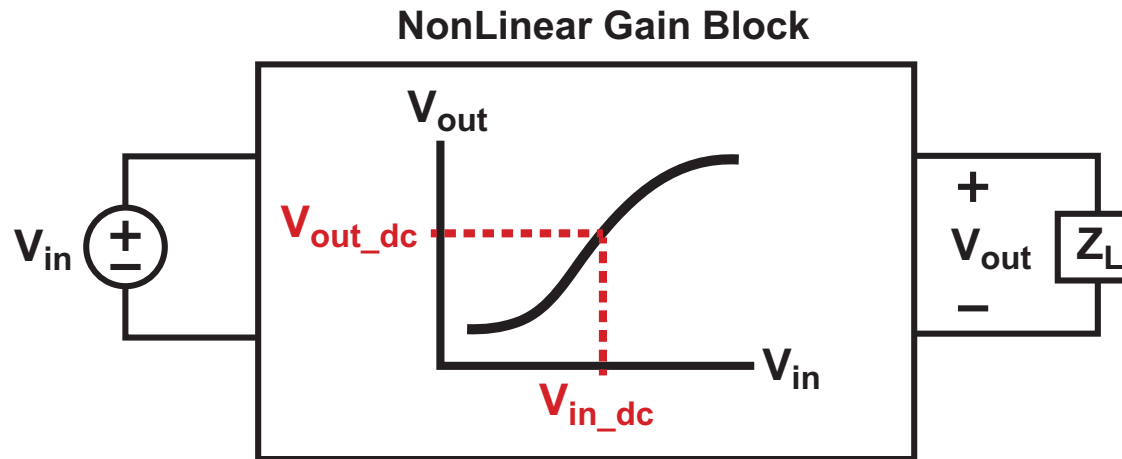
# Impact of Operating Point on Small Signal Modeling



- Sketch  $V_{out}$  versus  $V_{in}$  as the DC operating point is changed



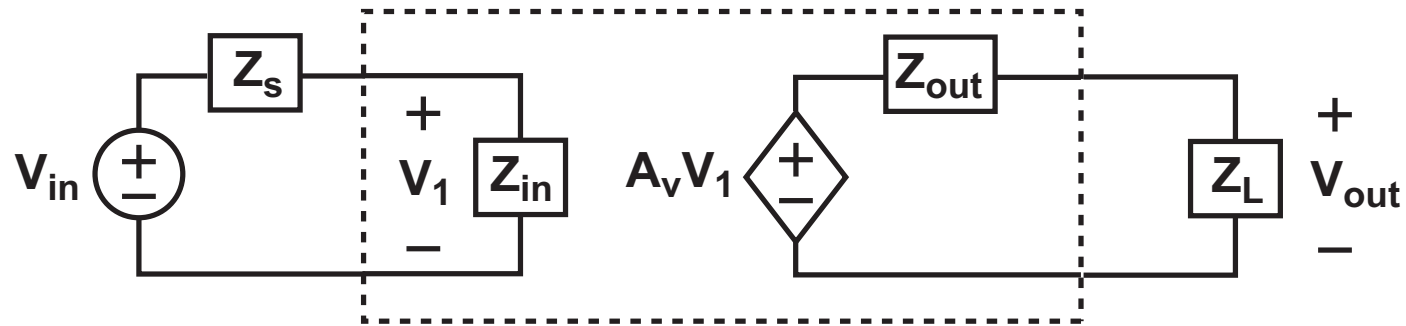
# Achieving a Small Signal Model



- Create a two port model of the above block

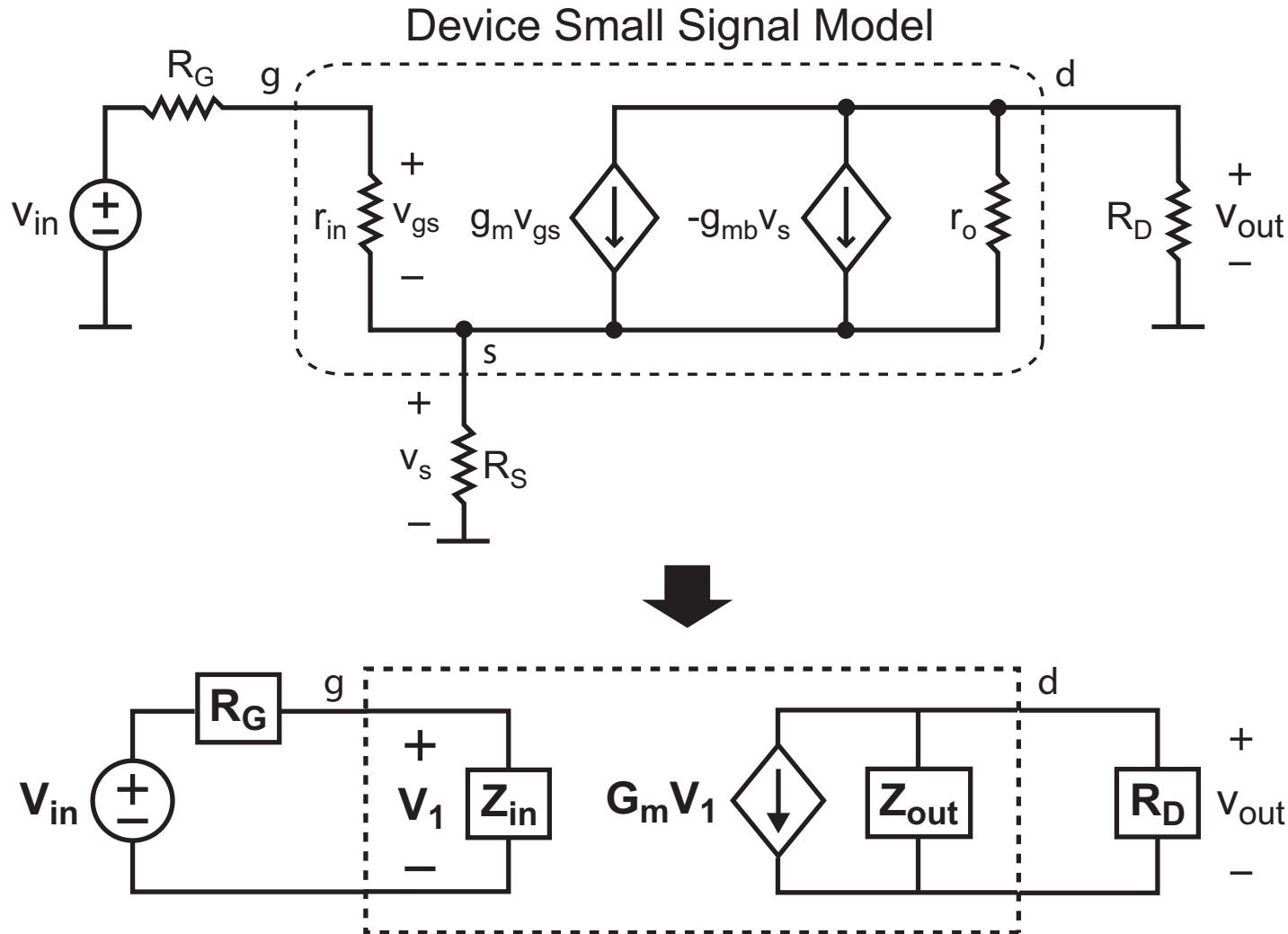
## Including Impedances in Two-Port Models

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- Compute  $V_{out}$  as a function of  $V_{in}$

## Example of Two-Port Derivation

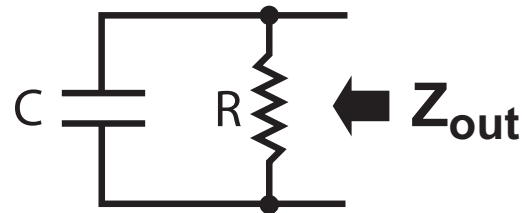
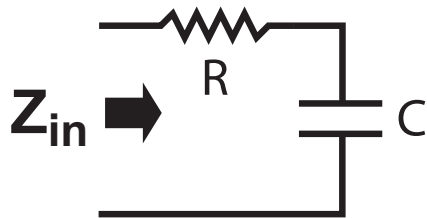
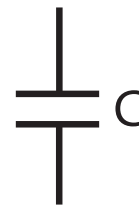


- Compute  $Z_{in}$ ,  $Z_{out}$ , and  $G_m$ 
  - Assume  $r_{in} = \text{infinity}$ ,  $g_{mb} = 0$

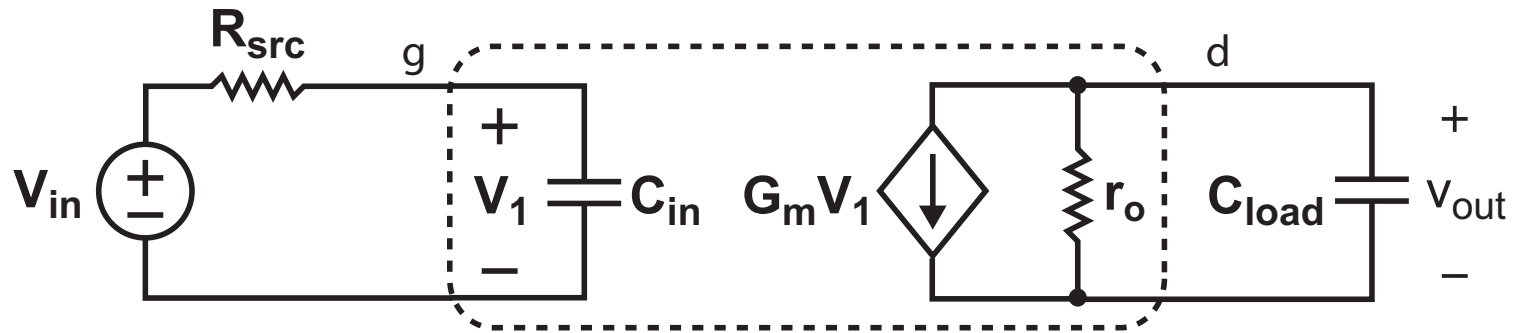
# Frequency Domain Modeling of Impedances

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- Determine Laplace Transform of Impedances Below:



## Example: Transfer Function of Two-Port Circuit



- Derive the transfer function  $V_{out}(s)/V_{in}(s)$
- Label the poles and zeros of the transfer function

# Frequency Response

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- Frequency response is readily derived from a transfer function:
  - For  $w$  (rad/s), you substitute  $s = jw$
  - For  $f$  (Hz), you substitute  $s = j2\pi f$
  - Note that  $j = \text{sqrt}(-1)$
- Example, for the transfer function on the previous page, the frequency response (in  $f$  (Hz)) is:

# Bode Plot Basics

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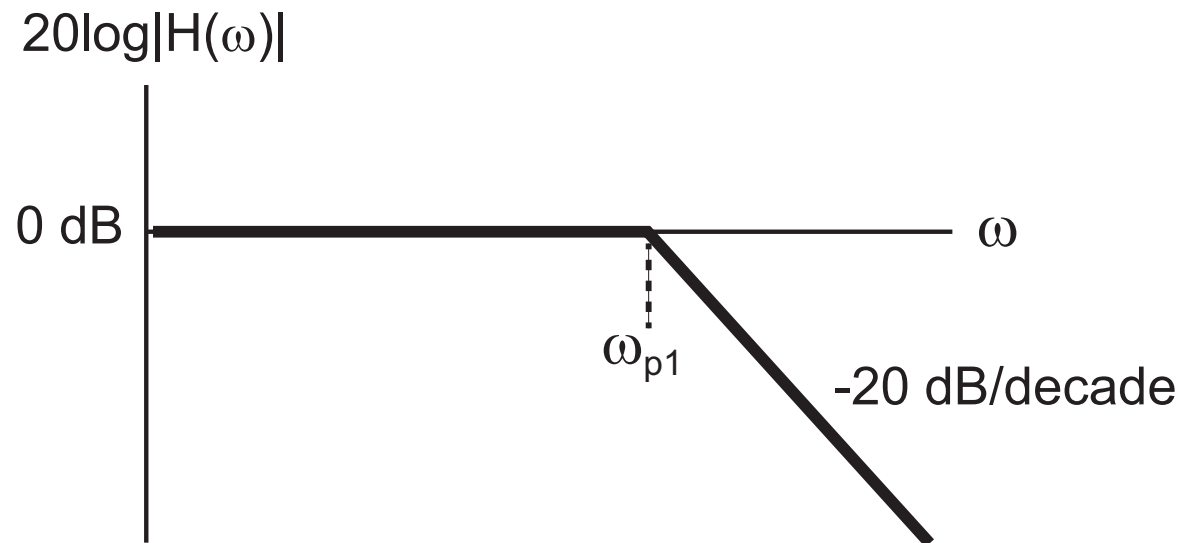
- The magnitude and phase of the frequency response is often depicted in the form of a Bode plot
- **Example:** 
$$H(\omega) = \frac{V_{out}(\omega)}{V_{in}(\omega)} = \frac{1 + j\omega/\omega_z}{(1 + j\omega/\omega_{p1})(1 + j\omega/\omega_{p2})}$$
  - **Log of magnitude (dB):**  $20 \log |H(\omega)|$   
$$= 20 \log |1 + j\omega/\omega_z| - 20 \log |1 + j\omega/\omega_{p1}| - 20 \log |1 + j\omega/\omega_{p2}|$$
    - Taking the log allows the poles and zeros to be plotted separately and then added together
  - **Phase:**  $\angle H(\omega)$   
$$= \angle(1 + j\omega/\omega_z) - \angle(1 + j\omega/\omega_{p1}) - \angle(1 + j\omega/\omega_{p2})$$
    - Phase of poles and zeros can also be plotted separately and then added together

# Plotting the Magnitude of Poles

- Plot the magnitude response of pole  $w_{p1}$

$$20 \log |H(w)| = 20 \log \left| \frac{1}{1+jw/w_{p1}} \right| = -20 \log |1 + jw/w_{p1}|$$

- For  $w \ll w_{p1}$ :  $20 \log |H(w)| \approx -20 \log |1| = 0$
- For  $w \gg w_{p1}$ :  $20 \log |H(w)| \approx -20 \log |w/w_{p1}|$





# Plotting the Magnitude of Zeros

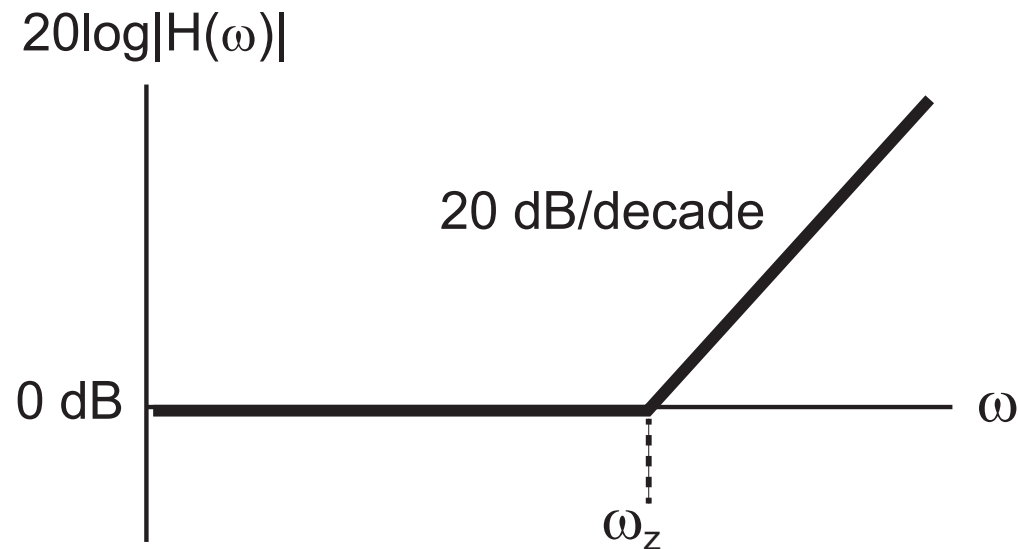
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- Plot the magnitude response of pole  $w_z$

$$20 \log |H(w)| = 20 \log |1 + jw/w_z|$$

- For  $w \ll w_z$ :  $20 \log |H(w)| \approx 20 \log |1| = 0$

- For  $w \gg w_z$ :  $20 \log |H(w)| \approx 20 \log |w/w_z|$

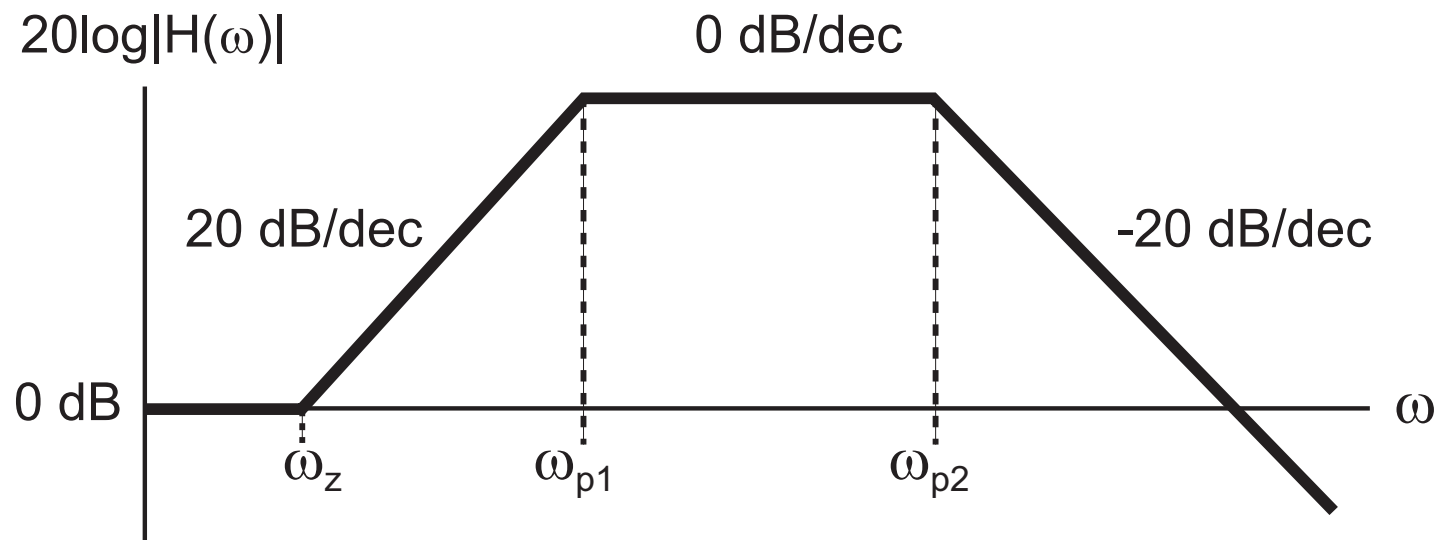


# Putting It All Together

## ■ Example Frequency Response:

$$H(\omega) = \frac{V_{out}(\omega)}{V_{in}(\omega)} = \frac{1 + j\omega/\omega_z}{(1 + j\omega/\omega_{p1})(1 + j\omega/\omega_{p2})}$$

- Assume  $\omega_z \ll \omega_{p1} \ll \omega_{p2}$



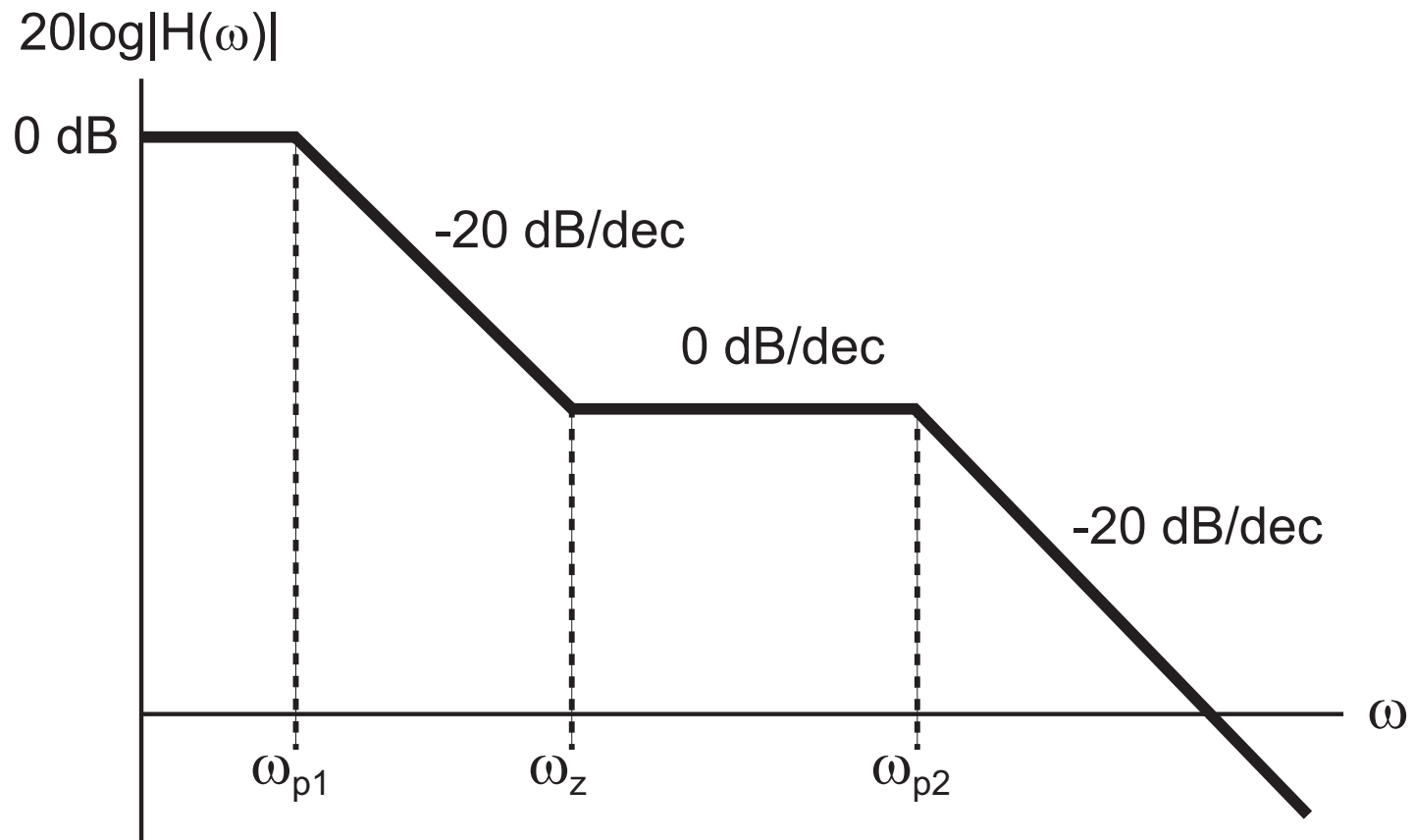
- What happens if  $\omega_{p1} \ll \omega_z \ll \omega_{p2}$  ?

# Changing the Order of Poles and Zeros

## ■ Example Frequency Response:

$$H(\omega) = \frac{V_{out}(\omega)}{V_{in}(\omega)} = \frac{1 + j\omega/\omega_z}{(1 + j\omega/\omega_{p1})(1 + j\omega/\omega_{p2})}$$

- Assume  $\omega_{p1} \ll \omega_z \ll \omega_{p2}$



# Changing the DC Gain from 1 to K

## ■ Example Frequency Response:

$$H(w) = \frac{V_{out}(w)}{V_{in}(w)} = K \frac{1 + jw/w_z}{(1 + jw/w_{p1})(1 + jw/w_{p2})}$$

- Assume  $w_{p1} \ll w_z \ll w_{p2}$

