

Analysis and Design of Analog Integrated Circuits
Lecture 5

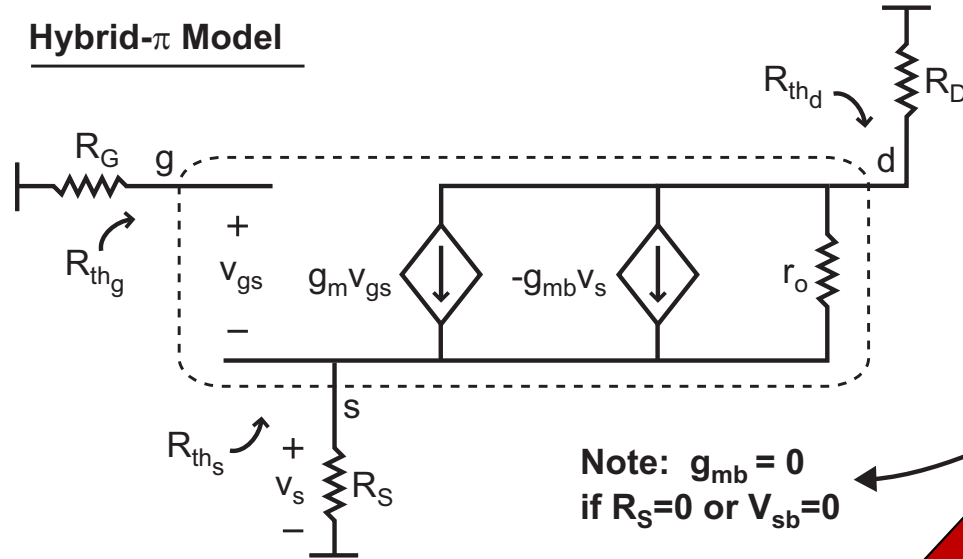
Single Stage Amplifiers

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From Lecture 4: Proposed Thevenin Model for Transistor

Hybrid- π Model

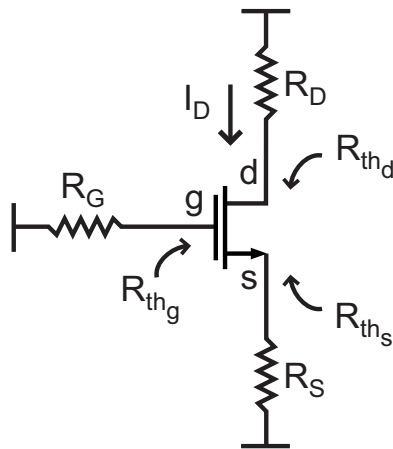


Note: $g_{mb} = 0$
if $R_S = 0$ or $V_{sb} = 0$

Key Small-Signal Parameters

Parameter	Strong Inversion	Weak Inversion
g_m	$\sqrt{2\mu_n C_{ox}(W/L)I_D}$	$\frac{qI_D}{nkT}$
g_{mb}	$\frac{\gamma g_m}{2\sqrt{2 \Phi_F + V_{SB}}}$	$\frac{(n-1)qI_D}{nkT}$
r_o	$\frac{1}{\lambda I_D}$	$\frac{1}{\lambda I_D}$

Thevenin Resistances



Exact

$$R_{thd} = r_o (1 + (g_m + g_{mb})R_S) + R_S$$

$$R_{thg} = \text{infinite}$$

$$R_{ths} = (1 + R_D/r_o) \left(r_o \parallel \frac{1}{g_m + g_{mb}} \right)$$

Approximation

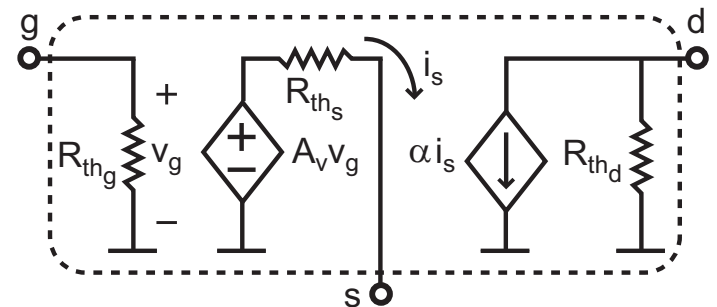
($g_{mb} \ll g_m$, $g_m r_o \gg 1$)

$$R_{thd} = r_o (1 + g_m R_S)$$

$$R_{thg} = \text{infinite}$$

$$R_{ths} = \frac{1 + R_D/r_o}{g_m} \approx \frac{1}{g_m} \quad (R_D \ll r_o)$$

Proposed Small Signal Transistor Model



Exact

$$A_v = g_m r_o \parallel \frac{g_m}{g_m + g_{mb}}$$

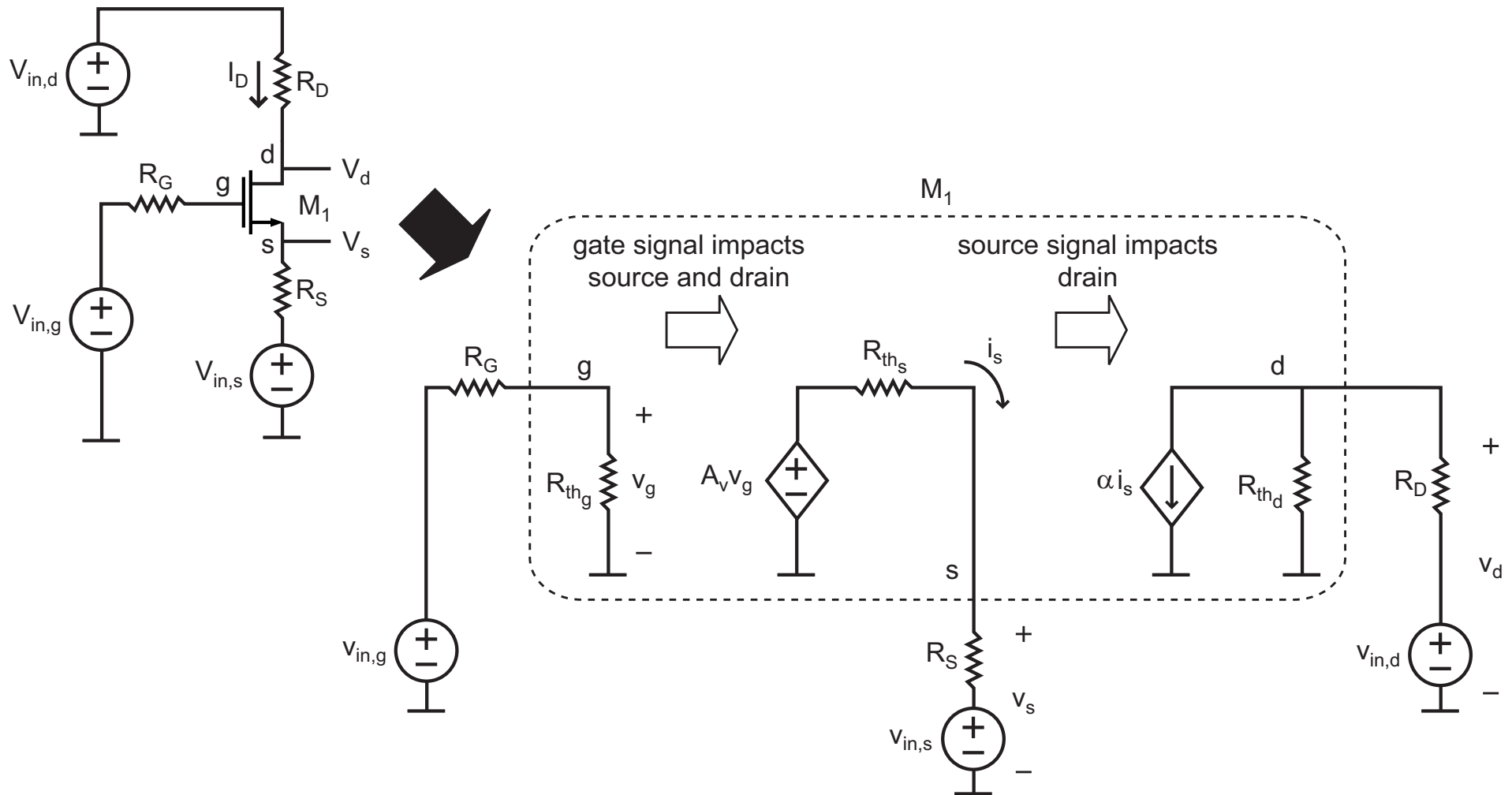
$$\alpha = 1 + R_D/R_{thd}$$

Approximation

$$A_v = 1 \quad (g_{mb} \ll g_m, g_m r_o \gg 1)$$

$$\alpha = 1 \quad (R_D \ll R_{thd})$$

A General View of Signal Flow in an Open Loop Device



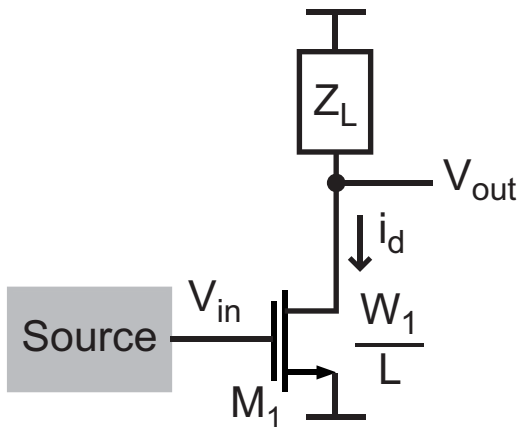
- To first order, influence of signals go from gate to source or from gate and/or source to drain
- This is only true when the device is in saturation

Why is a CMOS Transistor Useful?

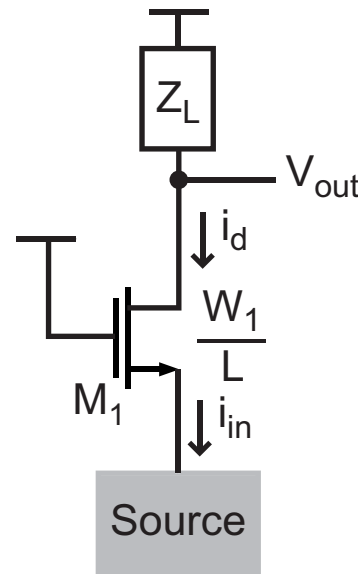
- **Key properties of a transistor:**
 - **Converts voltage to current**
 - **Funnels current between different impedance domains**
- **The above properties allow us to build amplifiers in creative ways**
 - **A number of circuit topologies are possible**
 - **A good designer can leverage the right topology to achieve the best performance for a given application**

Basic Single-Stage CMOS Amplifiers

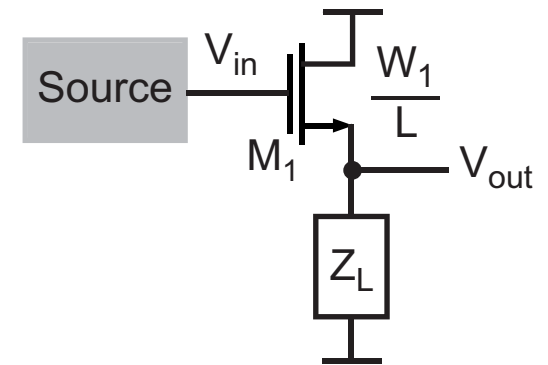
Common Source



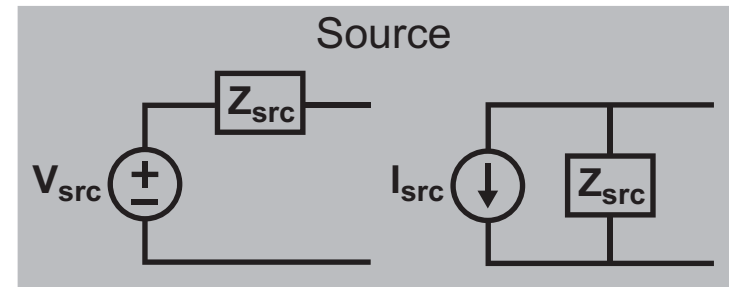
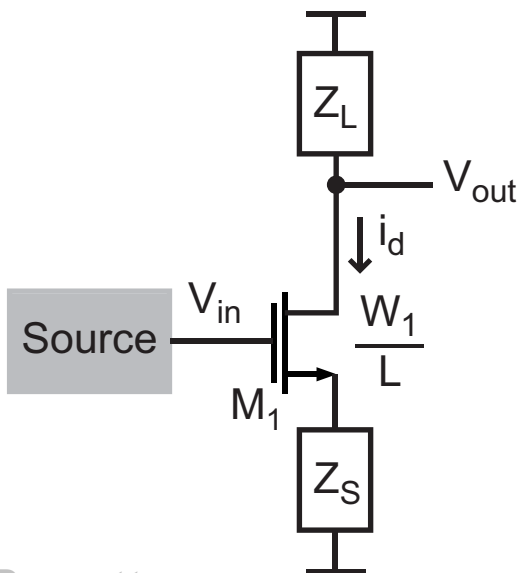
Common Gate



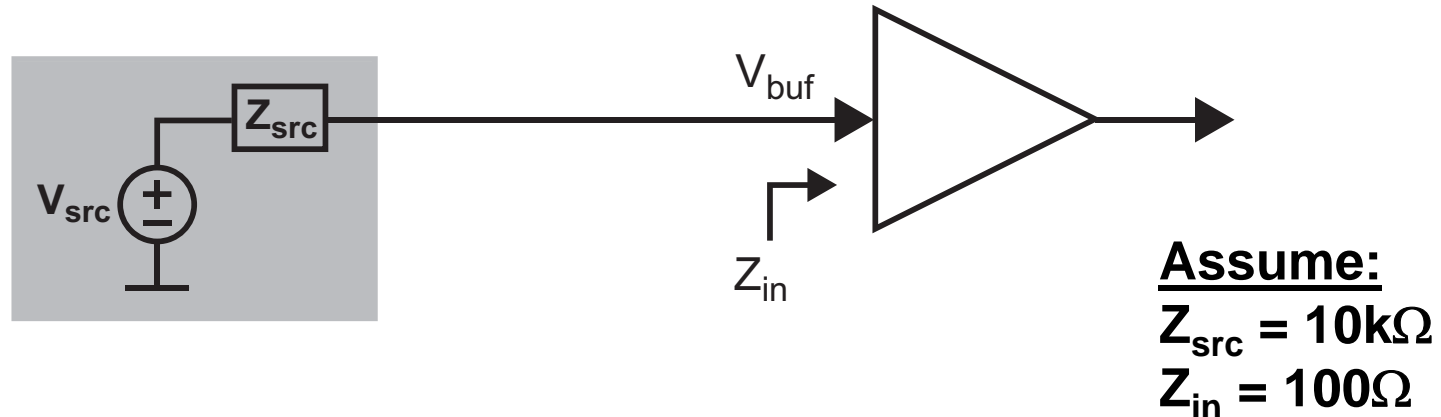
Source Follower



Common Source with Source Degeneration



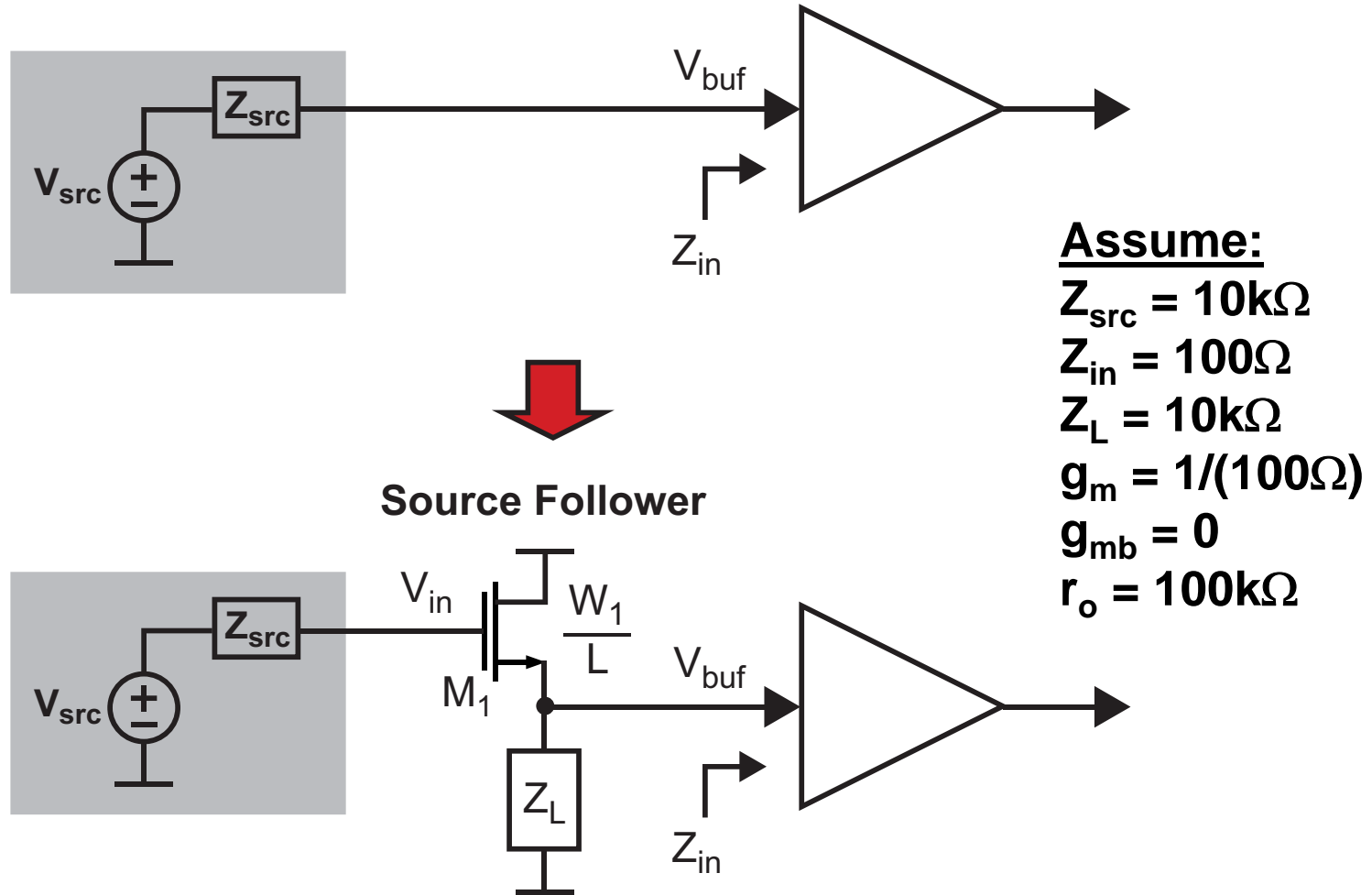
Example: The Impact of Low Input Impedance



- Here we consider how the gain is influenced by having a source with large impedance driving a circuit with low input impedance
 - Calculate the gain from V_{src} to V_{buf}
 - What is the impact of low Z_{in} and high Z_{src} ?

What type of amplifier stage would alleviate the impact of having high source impedance and low input impedance?

Consider a Source Follower Circuit



- Calculate the gain from V_{src} to V_{buf}
- How did the source follower improve the situation?

Example: The Impact of Low Source Impedance



Assume:

$$Z_{\text{src}} = 100\Omega$$

$$Z_{\text{in}} = 1\text{k}\Omega$$

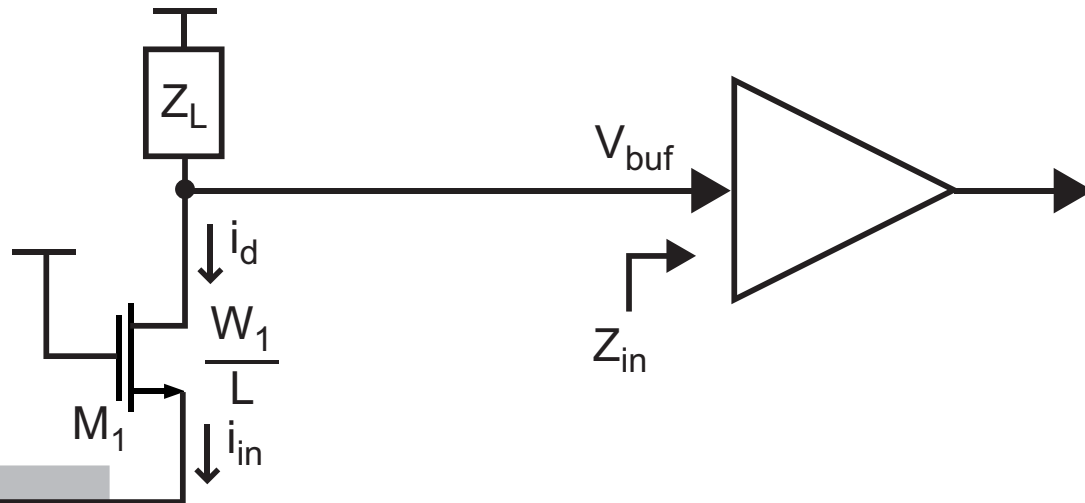
- Calculate the gain from I_{src} to V_{buf}
- What is the impact of low Z_{src} ?

What type of amplifier stage would alleviate the impact of having low source impedance?

Consider a Common Gate Amplifier



Common Gate



Assume:

$$Z_{src} = 100\Omega$$

$$Z_{in} = 1k\Omega$$

$$Z_L = 10k\Omega$$

$$g_m = 1/(100\Omega)$$

$$g_{mb} = 0$$

$$r_o = 100k\Omega$$

- Calculate the gain from I_{src} to V_{buf}

How can we further improve gain?

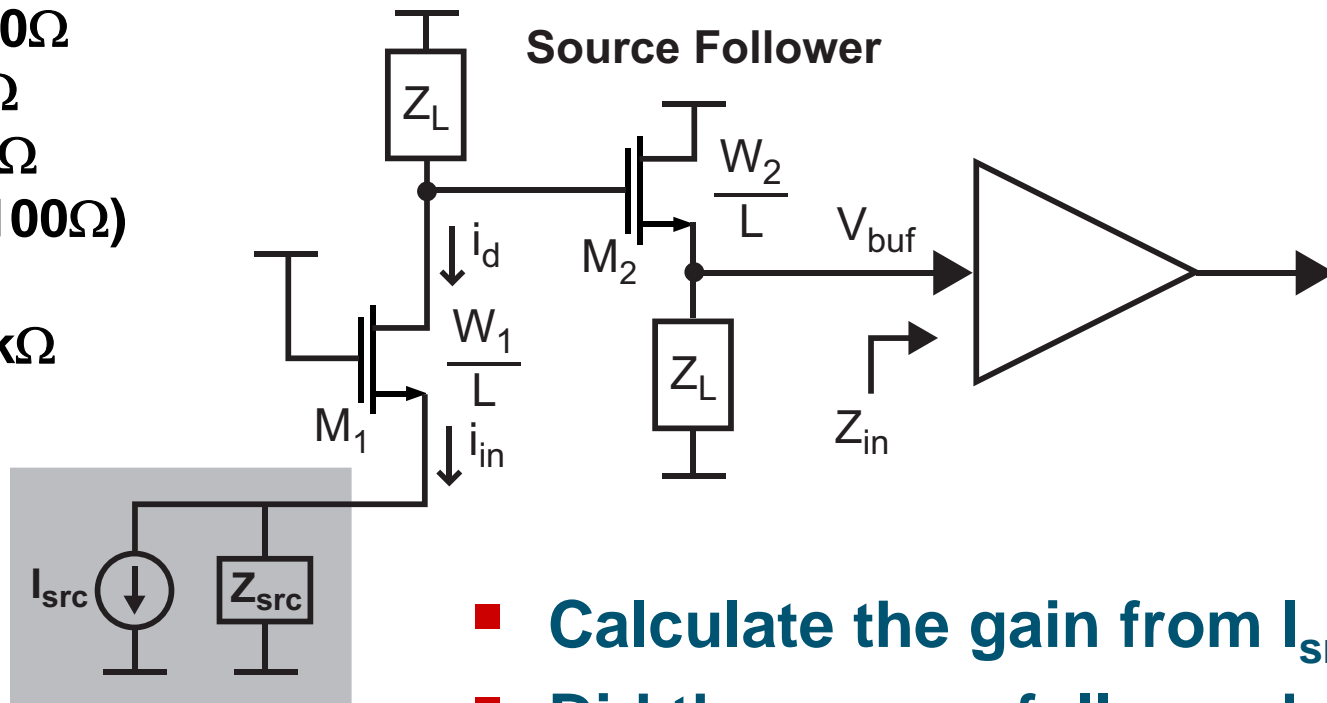
Add a Source Follower



Common Gate

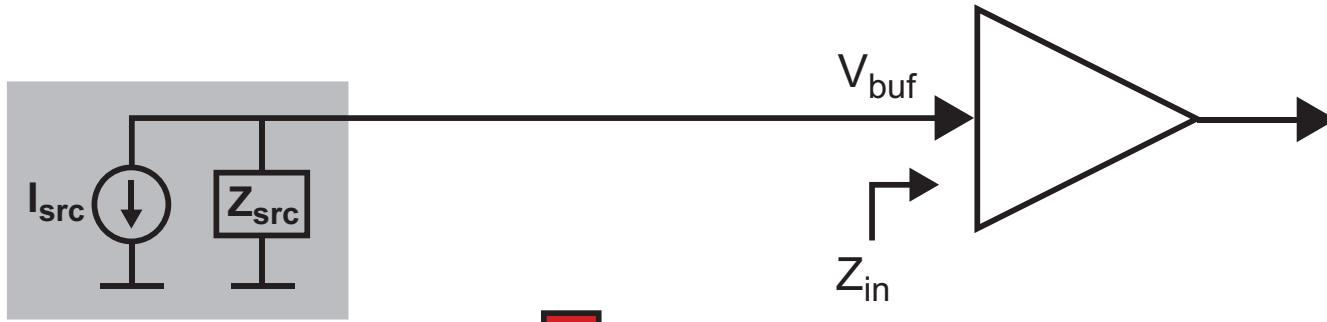
Source Follower

Assume:
 $Z_{src} = 100\Omega$
 $Z_{in} = 1k\Omega$
 $Z_L = 10k\Omega$
 $g_m = 1/(100\Omega)$
 $g_{mb} = 0$
 $r_o = 100k\Omega$



- Calculate the gain from I_{src} to V_{buf}
- Did the source follower help?

Consider Using a Common Source Amplifier Instead



Assume:

$$Z_{src} = 100\Omega$$

$$Z_{in} = 1k\Omega$$

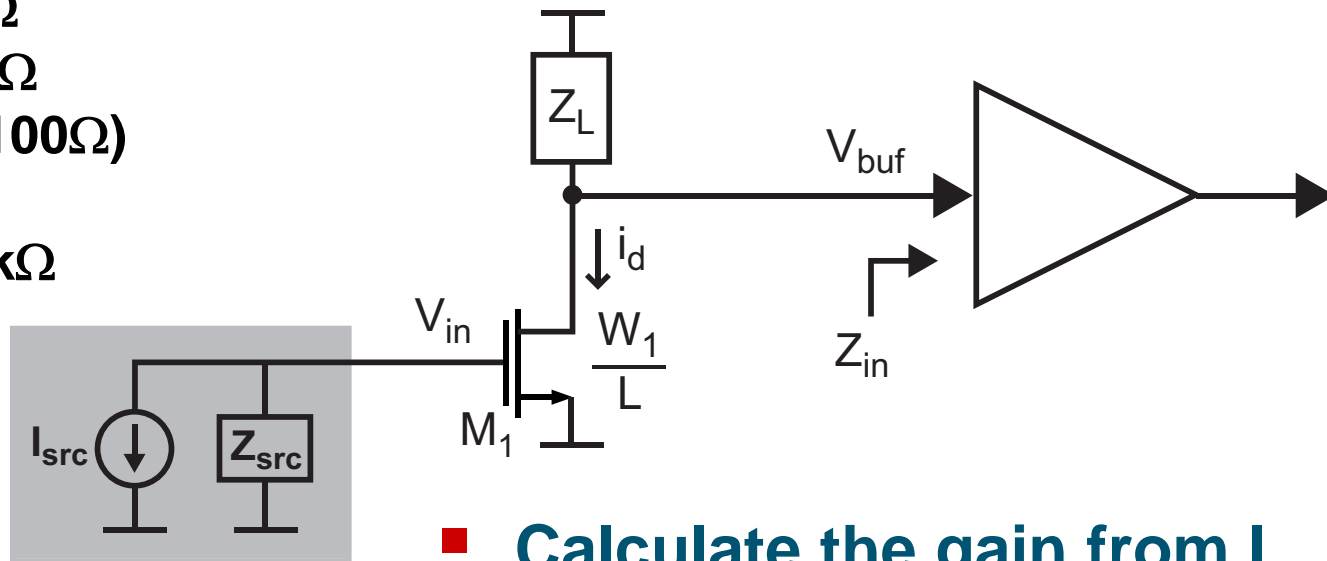
$$Z_L = 10k\Omega$$

$$g_m = 1/(100\Omega)$$

$$g_{mb} = 0$$

$$r_o = 100k\Omega$$

Common Source



- Calculate the gain from I_{src} to V_{buf}

How does the common gate approach compare to this?