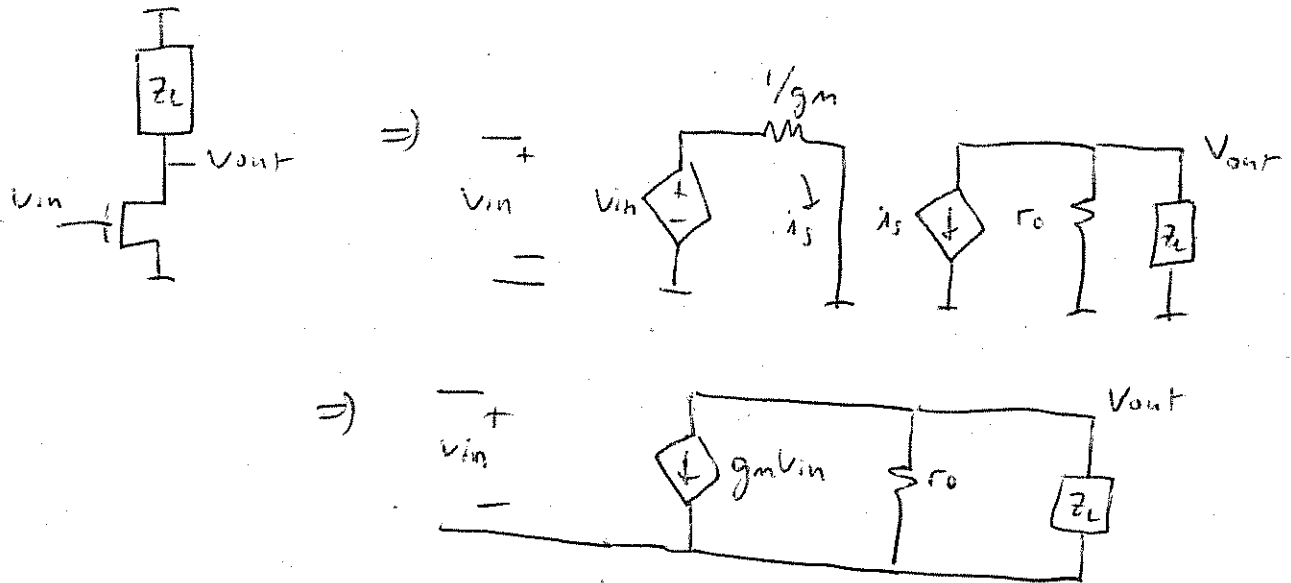


SLIDE 3) EXAMPLE GAIN CALCULATION FOR
COMMON SOURCE AMPLIFIER



$$\Rightarrow V_{out} = -(r_o \parallel Z_L) g_m V_{in}$$

$$\Rightarrow \boxed{\text{DC GAIN} = (-r_o \parallel Z_L) g_m}$$

$$\text{AS } Z_L \rightarrow \infty \Rightarrow \text{DC GAIN} \rightarrow -g_m r_o$$

SLIDE 6) BASED ON ANALYSIS ABOVE, SINCE CURRENT SOURCE BIAS HAS INFINITE OUTPUT IMPEDANCE

$$\Rightarrow Z_L = \infty$$

$$\Rightarrow \text{DC GAIN} \rightarrow \boxed{-g_m r_o}$$

SLIDE 8) BASED ON SLIDE 3 ANALYSIS ABOVE, FINITE Z_L ACTS TO REDUCE GAIN SINCE

$$\text{DC GAIN} = (-r_o \parallel Z_L) g_m$$

\Rightarrow WANT $|Z_L| \gg r_o$ TO AVOID GAIN REDUCTION

$$\text{FOR } M_3: I_{BIAS} = \frac{1}{2} \mu_p C_{ox} \frac{W_3}{L} (V_{SG} - |V_{THP}|)^2 (1 + \lambda V_{SD_3})$$

\Rightarrow THIS FORMULA HOLDS SINCE $V_{SD} = V_{SG} - |V_{THP}| + DV$

$$\Rightarrow V_{SD} > DV$$

\Rightarrow SATURATION

$$\text{FOR } M_2: I_D = \frac{1}{2} \mu_p C_{ox} \frac{W_2}{L} (V_{SG} - |V_{THP}|)^2 (1 + \lambda V_{SD_2})$$

\Rightarrow THIS FORMULA HOLDS SINCE V

$$\Rightarrow \frac{I_D}{I_{BIAS}} = \frac{\frac{1}{2} \mu_p C_{ox} \frac{W_2}{L} (V_{SG} - |V_{THP}|)^2 (1 + \lambda V_{SD_2})}{\frac{1}{2} \mu_p C_{ox} \frac{W_3}{L} (V_{SG} - |V_{THP}|)^2 (1 + \lambda V_{SD_3})}$$

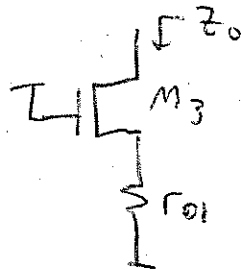
$$\boxed{\frac{I_D}{I_{BIAS}} = \left(\frac{W_2}{W_3} \right) \frac{1 + \lambda V_{SD_2}}{1 + \lambda V_{SD_3}}}$$

IF THE V_{DS} OF EACH PMOS DEVICE IS MATCHED,

THEN

$$\boxed{\frac{I_D}{I_{BIAS}} = \frac{W_2}{W_3}}$$

SLIDE 17:



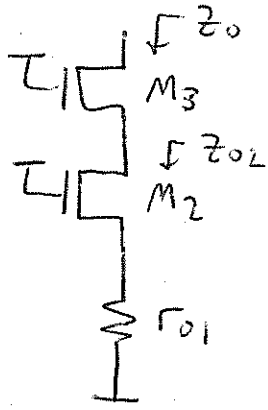
$$Z_D: R_{THO}|_{M_3} = r_{O3} (1 + (g_{m3} + g_{mb3}) r_{O1}) + r_{O1}$$

$$\approx \cancel{r_{O3}} \frac{g_m}{g_m} (r_{O3} g_{m3}) r_{O1}$$

\Rightarrow OUTPUT IMPEDANCE IS BOOSTED BY APPROXIMATELY $r_{O3} g_{m3}$ USING CASCODE TECHNIQUE

~~SLIDE 17:~~

SLIDE 18:



$$z_{O2} \approx (g_{m2} r_{O2}) r_{O1}$$

$$\Rightarrow z_O \approx (g_{m3} r_{O3}) (g_{m2} r_{O2}) r_{O1}$$